

Experimental Study on the Density-Driven Carbon Dioxide Convective Diffusion in Formation Water at Reservoir Conditions

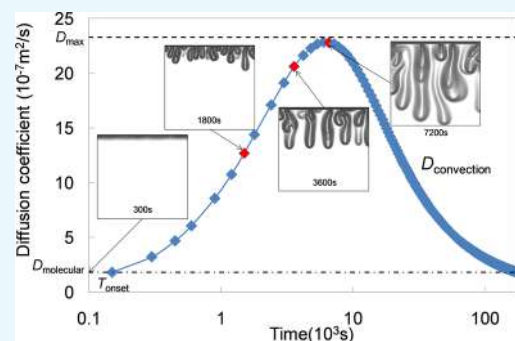
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ABSTRACT: Density-driven convection, which can accelerate the dissolution rate of carbon dioxide (CO₂) in resident brine, is critical for the long-term fate of the injected CO₂ permanence and security of CO₂ geological storage. Visualization experiments and pressure–volume–temperature (PVT) testing were conducted to investigate the influence from gravitational convection. For investigate gravitational instabilities and convective diffusion, we designed a Hele-Shaw cell rated to 70 MPa and Rayleigh number of 346 to conduct visualization experiments with the micro-schlieren technique. The average diffusion coefficient and time-dependent values were measured in the PVT experiments. We also calculated the convection parameters, including Rayleigh number and critical onset time, with a series of PVT testing at the temperature ranging 293.15–423.15 K and pressure ranging 14–24 MPa by using the constant-pressure method. Through visualization experiments, we observed convective currents triggered by the density gradient in the gas–liquid interface, which noticeably enhanced the CO₂ dissolution rate. The PVT testing confirmed that the diffusion coefficient increased sharply under the influence of the gravitational convection at the early stage and then decreased toward the average diffusion coefficient with time. The PVT testing also demonstrated the Rayleigh number increasing with temperature or pressure increasing under the reservoir conditions. The gravitational convection will be more likely to occur and more rapid with a greater pressure or higher temperature.



INTRODUCTION

Gravitational Convection. The growing concern about CO₂ emission urged people to investigate the solutions of CO₂ over emission. CO₂ geological storage in the aquifers or depleted oil reservoirs is one of the optimal techniques to prevent CO₂ from entering the atmosphere.^{1,2}

Dissolution trapping is an important mechanism, which usually captures two-thirds of the total storage volume.^{3,4} The molecular diffusion of CO₂ in brine is woefully slow.⁵ The key issue for accurate assessment of the dissolution trapping is the dissolution rate. As illustrated in Figure 1, many mechanisms accelerate the diffusion of CO₂ in brine and involve dispersion,⁶ advection, and gravitational convection.⁷

Among these mechanisms, advection is the dominant driving force because lower vertical permeability may reduce the gravitational convection while potentially increasing transverse mixing.⁹ Nevertheless, the gravitational convective diffusion can greatly enhance the CO₂ mixing efficiency, storage capacity, and mass transfer rate.¹⁰ Gravitational convection mitigates the risk of CO₂ leakage to provide a long-term storage security¹¹ by driving CO₂ sinking rather than rising to shallower formations. Therefore, gravitational convection is critical for the long-term fate of CO₂ and the security of storage.^{1,8}

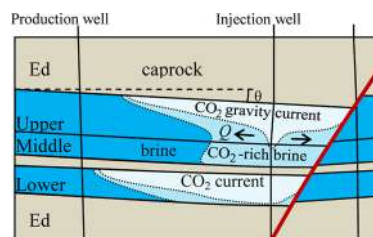


Figure 1. Schematic illustration of fluid dynamics and trapping associated with CO₂ geological storage in real formation, wherein the free CO₂ can be laterally displaced beneath the caprock⁸ by combinations of the volumetric flux of injected CO₂ (Q) and the aquifer slope (θ).

Convective Parameters. The CO₂ dissolution can result in a 2–3% density increase of brines;¹² the slight increment of density in brine will lead to gravitational instability^{9,13} and convection currents.^{10,14} Moreover, the convection will accelerate the dissolution of CO₂ into the brine, further enhance the mass transfer rate, and shorten the dissolution time.¹⁵ The density-driven convection is sometimes referred to

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as Rayleigh–Taylor instability.⁹ Based on the Boussinesq approximation, the density-driven flow can be described as a mixed equation of the mass conservation equation and Fick's second law¹⁶

$$\frac{\partial c(x, t)}{\partial t} + v \frac{\partial c(x, t)}{\partial x} - D \frac{\partial^2 c(x, t)}{\partial x^2} = 0 \quad (1)$$

where v is the velocity (or volume-averaged velocity).

The incompressible Navier–Stokes equation can describe the density-driven convective diffusion as

$$\frac{\partial v}{\partial t} = -\frac{1}{\rho} \nabla P + \frac{\mu}{\rho} \nabla^2 v + g \quad (2)$$

The most common criterion to indicate the occurrence of natural convection is Rayleigh number (Ra_c),¹⁷ which is a dimensionless measure as a ratio of free convection to diffusion^{7,8}

$$Ra = \frac{K \Delta \rho g H}{\phi \mu D} \quad (3)$$

where K is the effective permeability; $\Delta \rho$ is the excess density of CO₂-rich brine over fresh brine; g is the gravitational acceleration ($g = 9.8015 \text{ m/s}^2$ in Beijing); H is the vertical thickness of diffusion, which is less the height of model; ϕ is the porosity; μ is the viscosity of CO₂-rich brine; and D is the CO₂ diffusion coefficient.

For a Hele-Shaw cell with uniform aperture thickness, the porosity is 1, and its effective permeability can be calculated as^{18,19}

$$K = b^2/12 \quad (4)$$

where b is the aperture thickness of the Hele-Shaw cell.

Only when the diffusive layer becomes thick enough that the Rayleigh number exceeds a critical value (Ra_c); the gravitational instabilities can be triggered by perturbations in the diffusion layer.²⁰ Nield²¹ offered a method to measure the critical value under various boundary conditions. The critical Rayleigh number is 32.5 as estimated by Slim and Ramakrishnan²² based on the linear stability analysis, 55 as estimated by Szulczewski et al.,²³ and 31.5 as estimated by Slim²⁴ through the theoretical analysis of the dissolution rate. Some studies^{7,16,25} suggested that the appropriate critical value should be $4\pi^2$ with the associated critical wavenumber (λ_c) of π , which is also used in this paper.

A critical onset time (t_c) and critical wavelength (λ_c) were widely used to predict the gravitational instabilities. Both the onset time and critical wavelength depend on porosity and permeability.¹⁴

The critical onset time t_c can be predicted as²⁰

$$t_c = \alpha_1 D \left(\frac{\phi \mu}{K \Delta \rho g} \right)^2 \approx \alpha_2 Ra^{-2} \quad (5)$$

where α_1 and α_2 are the parameters for the onset time of convection. The parameter α_1 is 130 as reported by Hassanzadeh et al.²⁶ The parameter α_1 offered by Teng et al.^{27,28} is 48.7. We believe that the parameter α_1 should range from 45 to 130.

The critical wavelength λ_c can be calculated as

$$\lambda_c = \frac{a_3 D \phi \mu}{K \Delta \rho g} \quad (6)$$

It is reported that the density-driven convection enhances the CO₂ dissolution rate with the increase in Rayleigh number.²⁹ Islam et al.⁵ indicated that effective convection occurred only at a limited range of scales when Rayleigh numbers exceeded the critical value.

Hele-Shaw Experiments. Visualization study with the Hele-Shaw cell³⁰ apparatus is one of the primary methods used to investigate the mechanisms of the CO₂ natural convection. Kneafsey and Pruess²⁵ once performed CO₂ convective dissolution in transparent vertical Hele-Shaw cells that contained water overlain by a gas phase at atmospheric pressure. Backhaus et al.³¹ investigated the instability of initial convective dissolution with a Hele-Shaw cell ($6000 < Ra < 90000$) to determine the rates of CO₂ dissolution trapping in brine at atmospheric pressure. Slim et al.¹⁸ described the CO₂ convection behavior in brine from the first contact to 65% average saturation with a Hele-Shaw cell ($100 < Ra < 1700$) at atmospheric pressure. Mojtaba et al.³² observed the convective instabilities of CO₂ in a Hele-Shaw cell ($182 < Ra < 20860$) under 3.45 MPa. Vosper et al.³³ studied the process of CO₂ dissolution and convection in water under low pressure with a Hele-Shaw cell filled with transparent glass beads. Faisal et al.¹⁹ used a catalytic combustion-based total carbon analyzer to determine CO₂ mass transfer in a Hele-Shaw cell ($3277.88 < Ra < 36,420.87$) at atmospheric pressure. Vreme et al.³⁴ studied the gravitational instability triggered by CO₂ dissolution through a water–gas interface with a Hele-Shaw experiment. Lu et al.³⁵ invented a Hele-Shaw cell that can perform under a high gas pressure of 10 MPa, and experimental results only in the atmosphere pressure were exhibited. Tani³⁶ established the classical solvability of the one-phase Hele-Shaw problem and justified the vanishing coefficient of the time derivative in the parabolic equation based on Hele-Shaw cell experiments at low pressure. Thomas et al.³⁷ conducted CO₂ convective dissolution in a Hele-Shaw cell and found that the increase in the salt concentration hindered the development of the instability, increased the wavelength of the convective pattern, and decreased the growth rate and velocity of fingers. Mahmoodpour et al.³⁸ designed a novel Hele-Shaw cell ($2919 < Ra < 4841$) and presented the first experiments of dissolution-driven convection of CO₂ in a confined brine-saturated porous medium at pressures up to 3.69 MPa (535.3 psi).

One key issue for the convection experiment with Hele-Shaw cell is the way to detect the variations of CO₂ concentration for visualization purposes. The traditional acid–base indicators cannot capture the full extent of the convection.³⁹ The research on color indicator demonstrated that the observed patterns and the instabilities may not depend on the presence of a color indicator.^{40,41} However, most of the studies visualizing convective patterns with color indicators ignore the concentration.³⁹

Micro-schlieren technique is sensitive to the CO₂ concentration based on the deflection of light by a refractive index gradient.⁴² Through comparison between the reference and shadowgraph, the noise has been reduced, and the contrast has been improved. The shadow pattern is a light-intensity representation of the low-density regions and high-density regions, which characterizes the well-defined convective flow.⁴³

The schlieren images can reflect the changes in the refractive index (n) that is directly related to the density gradient. The relation between density (ρ) and refractive index is described by using the Gladstone–Dale relation⁴⁴

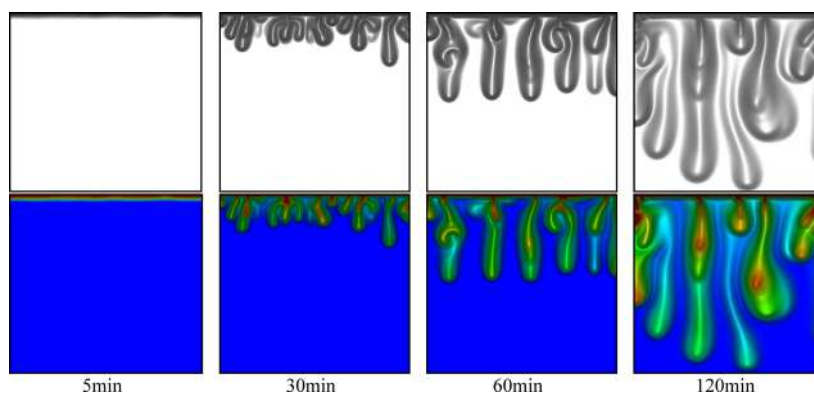


Figure 2. Schlieren images and color schlieren density images of gravitational convection in the Hele-Shaw cell after 5, 30, 60 and 120 min. The view fields of all figures are 1 cm × 1 cm. Blue indicates fresh brine, and the color turns from blue to red with the increase in CO₂ concentrations.

$$n = K_p \rho + 1 \quad (7)$$

where n is the refractive index, ρ is the density, K_p and K_C are the Gladstone–Dale constants, K_p reflects the physical refractive energy, and K_C reflects the chemical refractive energy of fluid. The Gladstone–Dale compatibility, $1 - (K_p/K_C)$, is 0.037 for the ideal formula.

$$K_C = C_i k_i \quad (8)$$

where C_i is the weight percentage of each constituent, and k_i are the specific constants of the chemical data.

PVT Testing. There are a few experimental studies about the convective diffusion in the pressure–volume–temperature (PVT) cell at reservoir conditions.³ Yang and Gu⁴⁵ calculated the CO₂ mass transfer rate in resident brine with a visual high-pressure PVT cell and the pressure decay method. Mojtaba et al.³² performed quantitative experiments with the PVT cell at elevated pressure and provided an estimation of the convective dissolution of CO₂ in brine. Khosrokhavar³ studied the CO₂ transfer rate for both fresh brine and brine in pressure constant experiments. The results revealed that the mass transfer rate was much faster than the prediction by Fick's law in the absence of natural convection.

Based on the conservation laws, the total amount of dissolved CO₂ can be calculated as follows

$$n_t = \frac{PV_0}{ZRT} - \frac{PV_t c_t}{ZRT} - \frac{PV_s}{RT} \sum_{t'=0}^t \frac{c_{t'}}{Z} \quad (9)$$

where P is the pressure of supercritical fluid in the PVT cell; V_0 and V_t are volumes of supercritical fluid or gas at time 0 and t , respectively; V_s is the sampling volume; c_0 and c_t are concentrations of CO₂ in supercritical fluid or gas at time 0 and t , respectively; Z is the compressibility factor of supercritical fluid or gas; R is the universal gas constant (8.3145 J/(mol·K)); T is the temperature; and t is the diffusion time.

For the pure Fickian diffusion, many researchers^{18,46,47} derived separately a same relationship between the mole number of dissolved CO₂ and diffusion coefficient

$$n_t = 2C_s A \sqrt{Dt/\pi} \quad (10)$$

where n_t is the mole number of dissolved CO₂ at time t ; A is the area of gas–liquid interface; C_s is the molar concentration or molarity of saturated CO₂ dissolved in liquid. The concentration C_s of saturated CO₂ can be obtained by the following relation

$$C_s = \frac{c_t n_s}{V_s} = \frac{c_t P_0 V_{s0}}{RT_0 V_s} \quad (11)$$

where n_s is the mole number of gas released from the sample at atmospheric pressure, P_0 is the atmospheric pressure, V_{s0} is the volume of the released gas, and T_0 is the temperature of water bath.

According to eq 10, the time-dependent diffusion coefficient was calculated as

$$D = \frac{\pi}{4t} \left(\frac{n_t}{C_s A} \right)^2 \quad (12)$$

Chemical Potential and Reaction Equilibrium. The chemical potential of gaseous or supercritical CO₂ (scCO₂) is⁴⁸

$$\mu(g) = \mu^\theta(g) + ZRT \ln(P/P^\theta) + \int_{P^\theta}^P (V - ZRT) dP \quad (13)$$

where $\mu(g)$ is the chemical potential of supercritical CO₂, and $\mu^\theta(g)$ is the standard chemical potential, and P^θ is the standard pressure.

The chemical potential of CO₂ in aqueous solution is

$$\mu(\text{aq}) = \mu^\theta(\text{aq}) + RT \ln(c/c^\theta) \quad (14)$$

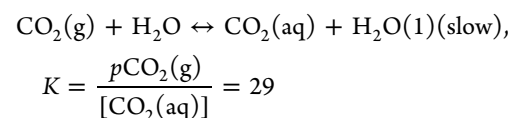
Gibbs free energy of solution is⁴⁸

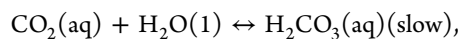
$$G = c_{\text{CO}_2} G_{\text{CO}_2} + c_{\text{H}_2\text{O}} G_{\text{H}_2\text{O}} + \Delta H_{\text{mix}} - T \Delta S_{\text{mix}} \quad (15)$$

where G is the Gibbs free energy, ΔH_{mix} is the enthalpy change, and ΔS_{mix} is the entropy change. The traditional thermodynamic formula is

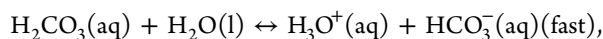
$$\Delta S_{\text{mix}} = -R(c_{\text{CO}_2} \ln c_{\text{CO}_2} + c_{\text{H}_2\text{O}} \ln c_{\text{H}_2\text{O}}) \quad (16)$$

CO₂ has much weaker hydrogen bonding than H₂CO₃ to H₂O.⁴⁹ When CO₂ dissolves in water, CO₂ undergoes a slight hydration (~0.26%) to H₂CO₃ (O=C(OH)₂), results in acidic H₂CO₃ ionization, and produces a number of carbonate ions with the following chemical equilibria²

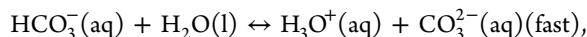




$$K = \frac{[\text{CO}_2(\text{aq})]}{[\text{H}_2\text{CO}_3]} = 590$$



$$K = \frac{[\text{H}_3\text{O}^+][\text{HCO}_3^-]}{[\text{H}_2\text{CO}_3]} = 0.25 \text{ mM}$$



$$K = \frac{[\text{H}_3\text{O}^+][\text{CO}_3^{2-}]}{[\text{HCO}_3^-]} = 0.047 \text{ nM}$$

RESULTS AND DISCUSSION

Visualization Experiments. Figure 2 illustrates the convection processes in the Hele-Shaw experiments. The results were visualized using an optical shadowgraph, which imaged the variation of density via the refraction index.

In the Hele-Shaw experiments, CO_2 started to dissolve as soon as it contacted with the resident brine. The brine with dissolved CO_2 has a higher density than fresh brine.³ The density of fresh formation water tested with density meters (Anton Paar, DMA HP) is 1.0036 g/mL under reservoir conditions, and the density of CO_2 -saturated brine is 1.0275 g/mL. The small increase in brine density is critical to forming convection. It is well known that the Rayleigh–Taylor instability occurs when high-density fluid suspends over lower-density fluid in a gravitational field.^{50–52} With the increase in CO_2 concentration, the density increases, which can finally lead to gravitational instabilities in the system.²³

At the initial stage, the CO_2 dissolution occurred via diffusion on the gas–liquid interface without convection. With the increase in CO_2 concentration in the top fluid, a high-dense planar layer formed and widened rapidly at an almost constant rate. Considering the critical Rayleigh number (Ra_c) as $4\pi^2$, the theoretical critical thickness of the diffusive layer (H_c) is 9.1156 mm, and the corresponding onset time (t_c) is in the range of 2.159–6.238 min. As explained before, convection is impossible when the thickness of the diffusive layer exceeds the critical value.²³ Meanwhile, the gravitational instabilities generated led to tiny disturbances in the diffusive layer sooner.

About half an hour later, the disturbances in the diffusive layer gradually boosted and expanded into distinct plumes under the gravitational instabilities.⁵³ There was no clear demarcation between the disturbances and plumes. The length of the frontal plumes was measured each time (see Figure 2). The plume length increased with time in nearly linear rather than accelerated transport.

One hour later, the convective plumes were tightly packed with hazy edges when Rayleigh–Taylor convections had developed spontaneously.^{18,50} In this step, the plumes carrying CO_2 grew downward and propagated to form many branches and lobes. Meanwhile, most branches died away, and most lobes broke up as CO_2 diffused into the surrounding brine (see Figure 2). With the occurrence of convection, the CO_2 dissolution rate will increase, and the leakage risk will decrease.¹⁰ The width of each plume is varied considerably along the length of the plume, particularly under Rayleigh–Taylor instability. Because Rayleigh–Taylor instability lacks

good repetition, we paid more attention to the qualitative law of gravitational convection in the visualization experiments.

Two hours later, the CO_2 -dissolved brine vertically streamed down more stably, and the fluid with low CO_2 concentration floated to the top by gravity. The density contrast between CO_2 -saturated brine and initial brine is the driving force of plume migration due to the gravitational instabilities.⁵ Because the density-driven convection can reduce CO_2 concentration in the gas–liquid interface,³¹ the dissolution rate was also enhanced considerably.³³ With the broadening of the convective plumes and the growing amount of CO_2 -dissolved brine filling the bottom, the CO_2 concentration at the bottom part of the liquid was noticeably higher than other parts. The boundaries of convective plumes at the bottom blurred gradually to obscurity first. The convective diffusion slowly fell into a decline from bottom to top. Finally, the convective schlieren disappeared as the gravitational convection abated, and the image recovered to the original background.

The visualization experiments illustrated that the gravitational convection creates a more efficient dissolving process by bringing the fresh brine upward to the interface to touch scCO_2 . The natural convection speeds up the CO_2 dissolution. The gravitational convection plays a significant and positive role in CO_2 geological storage capacity and safety.^{27,54}

Influence of Convection on Diffusion Coefficients.

Assuming that the diffusive flux is governed by Fick's law with the idealized mass conservation in the PVT system, the saturated solubility of CO_2 in formation water is 5.68×10^{-4} mol/mL under the reservoir conditions (355.65 K, 20.2 MPa). The volume alterations of the supercritical CO_2 with time in the PVT system are shown in Figure 3.

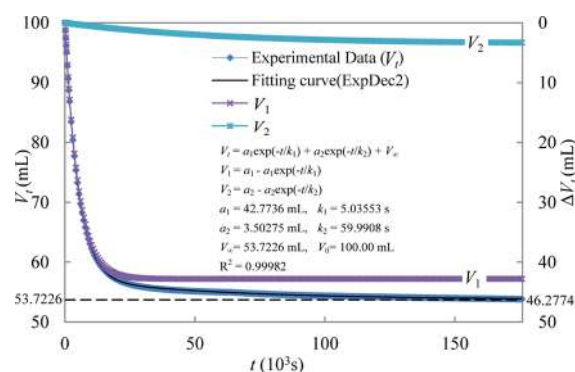


Figure 3. CO_2 volume changed with time during the CO_2 diffusion experiment. The actual value of CO_2 volume in the PVT experiments matches well with the ExpDec2 model,⁵⁵ where V_1 is the CO_2 volume at time t , t is the diffusive time, a_1 and a_2 are the volume coefficients of the fitting formula, and k_1 and k_2 are the time coefficients of the fitting formula.

In the Fickian diffusion process, CO_2 diffuses into brine and forms a diffusive boundary layer¹¹ that grows in proportion to the square root of time (\sqrt{t}), where perturbations to the stable layer are damped.⁵ The relationship curve between the mole number of CO_2 dissolved in resident brines (n_t) and the root of time (\sqrt{t}) is drawn in Figure 4.

The curves in Figure 4 are flatter at the initial stage, which indicated that the diffusion was mainly the Fickian diffusion. A study⁴⁵ reported that the appearance is caused by gas compression. But the compression has seldom affected our experiments because CO_2 had been pressurized under

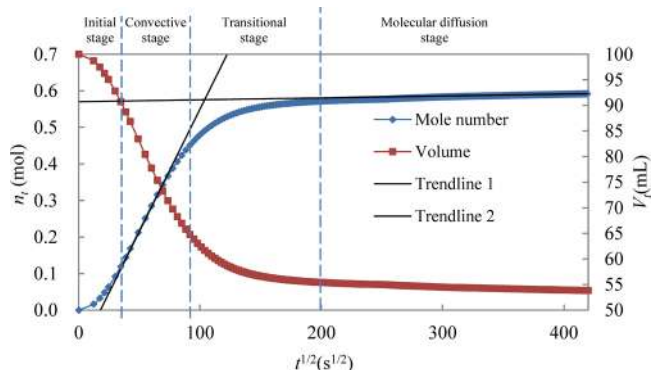


Figure 4. Mole number of CO₂ dissolved in 1 L of brine against the root of time.

experimental conditions before injecting. The CO₂ diffusion flux (J_t) was dramatically enhanced at the early stage. The diffusion of CO₂ was a faster process at this stage. The CO₂ diffusion coefficient decreased from a maximum of $2.3095 \times 10^{-6} \text{ m}^2/\text{s}$. The spontaneous convection was considered as the main cause of the acceleration in the CO₂ diffusion rate at the beginning.¹⁸ The dissolution rate slowed down gradually at the transitional stage. The average CO₂ diffusion coefficient is $1.803 \times 10^{-7} \text{ m}^2/\text{s}$.

The ExpDec2 model can be applied to analyze the data from constant-pressure experiments also. We calculate the diffusion coefficient by fitting pressure-decay data in Figure 3 with this model^{55,56}

$$D = 4H^2/k\pi^2 \quad (17)$$

where k are the coefficients of Zhao's fitting formula⁵⁶ obtained by fitting pressure-decay data.

We divide the changes of volume into two parts (Figure 3): V_1 reflects the convective diffusion more, and V_2 is prone to reflect the molecular diffusion. V_1 changed rapidly, and its contribution to diffusion reached 92.4287%. However, variation of V_1 had moderated abruptly after a dozen of hours. V_2 changed placidly and sustainably. Based on eq 17, the diffusion coefficient (D_2) calculated by using k_2 is $1.803 \times 10^{-7} \text{ m}^2/\text{s}$, which is similar to the average CO₂ diffusion coefficient. The diffusion coefficient (D_1) calculated by using k_1 is $2.328 \times 10^{-6} \text{ m}^2/\text{s}$.

The time-dependent diffusion coefficient was calculated by the formula

$$D = \frac{\pi H^2}{4t} \left(\frac{V_0 - V_t}{V_0 - V_\infty} \right)^2 \quad (18)$$

According to eqs 12 and 18, the diffusion coefficients were calculated.^{18,46} The time-dependent diffusion coefficient curves were drawn in Figure 5.

The CO₂ diffusion coefficient reached a peak of $2.282 \times 10^{-6} \text{ m}^2/\text{s}$ rapidly in the initial period and then dropped below the average diffusion coefficient of $1.803 \times 10^{-7} \text{ m}^2/\text{s}$ (Figure 5). The peak diffusion coefficient is more than D_1 and less than the sum of D_1 and D_2 . This means that natural convection decreases with time, similar to the density gradient.

Compared with the molecular diffusion coefficient, the average diffusion of CO₂ in brine has improved. Apart from the Fickian diffusion, the average diffusion coefficient of CO₂ is also controlled by chemical reactions and dispersion.⁵⁷ Table 1

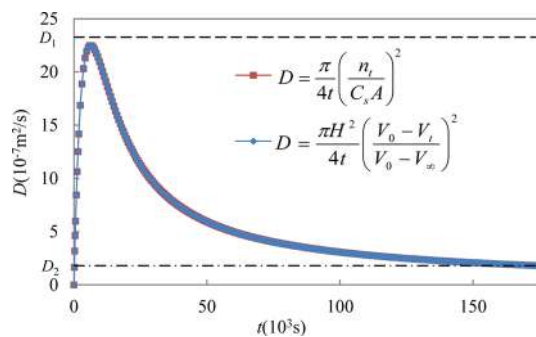


Figure 5. Time-dependent diffusion coefficient curves.

lists the diffusion coefficients of different ions calculated on the basis of the data reported by Ellis et al.⁵⁸

Effect of Pressure on Gravitational Convection. Table 2 presents the CO₂ saturated solubility (C_s), density (ρ), compressibility factor (Z), volumetric factor (V_f/V_s), average diffusion coefficient (D_a), molecular diffusion coefficient (D_m), normalized Rayleigh number (Ra), and normalized critical time (t_c) in the PVT experiments under pressures in the range of 14–24 MPa.

The saturated solubility of CO₂ in brine increased with pressure. Henry's law indicates that the gaseous CO₂ solubility is linear with respect to pressure. Upon exceeding the critical pressure (7.383 MPa), the solubility of supercritical CO₂ increased sharply with pressure. For the pressure in the range of 14–24 MPa, the elevated pressure enhances CO₂ solubility with lower increment (Table 2). This can be explained by CO₂ chemical potential energy. The chemical potential⁴⁸ of CO₂ in the supercritical state $\mu(\text{sc})$ increased with pressure greater than that in the melted state $\mu(\text{aq})$. The Gibbs energy decreases during elevating pressure ($\Delta G < 0$); more CO₂ molecules can diffuse spontaneously from the supercritical phase into the aqueous phase.

According to molecular dynamics, the molecular diffusion coefficient is proportional to the mean free path of a CO₂ molecule, which decreased with pressure ($D_m \propto P^{-1}$). For self-diffusion at different pressures but the same temperature, the following empirical equation has been suggested⁵⁹

$$\frac{D_m(P_1)}{D_m(P_2)} = \frac{\rho_g(P_2)}{\rho_g(P_1)} = \frac{Z(P_1)/P_1}{Z(P_2)/P_2} \quad (19)$$

where ρ_g is the density of CO₂, and P_1 and P_2 are the corresponding pressures.

The molecular diffusion coefficient (D_m) decreases with pressure. On the contrary, the average diffusion coefficient (D_a) increases with pressure (Table 2).

The density of CO₂-rich brine also increases with pressure. The CO₂ dissolution increasing with pressure is a main reason to increase the density of solution, although the volume also changes.

The pressure affects the density-driven convection.¹⁹ According to eq 1, the Rayleigh number depends on the excess density and diffusion coefficient, both of which are affected by pressure. The pressure has a larger influence on CO₂ solubility and density than diffusion coefficient at the reservoir conditions. Thus, the excess density increases with pressure to enhance the proneness to form gravitational convection.

Table 1. Molecular Diffusion Coefficients of Different Ions in Brine at 355.65 K

species	D_m ($\times 10^{-9}$ m ² /s)	species	D_m ($\times 10^{-9}$ m ² /s)	species	D_m ($\times 10^{-9}$ m ² /s)
H ⁺	27.23868	CO ₂	5.674726	HCO ₃ ⁻	3.627144
OH ⁻	15.38611	H ₂ CO ₃	4.387674	CO ₃ ²⁻	2.831513

Table 2. Experimental Parameters with Pressures in the Range of 14–24 MPa (355.65 K)

P (MPa)	C_s (10^4 mol/mL)	ρ (g/L)	Z	V_f/V_s	D_a (10^{-7} m ² /s)	D_m (10^{-9} m ² /s)	Ra	t_c
14.0	5.2940	1.0259	0.5854	1.0053	1.7767	9.0415	0.9449	1.1198
15.0	5.4286	1.0264	0.5639	1.0048	1.7823	8.1306	0.9662	1.0710
16.0	5.5289	1.0268	0.5485	1.0043	1.7875	7.4129	0.9813	1.0382
17.0	5.5951	1.0271	0.5380	1.0039	1.7903	6.8436	0.9914	1.0173
18.0	5.6338	1.0273	0.5318	1.0036	1.7931	6.3890	0.9965	1.0068
19.0	5.6612	1.0274	0.5292	1.0033	1.7977	6.0234	0.9989	1.0020
20.0	5.6795	1.0275	0.5297	1.0031	1.8024	5.7271	0.9997	1.0005
20.2	5.6840	1.0275	0.5308	1.0030	1.8039	5.6747	1.0000	1.0000
21.0	5.6999	1.0276	0.5326	1.0029	1.8060	5.4848	1.0011	0.9977
22.0	5.7159	1.0276	0.5376	1.0027	1.8095	5.2847	1.0023	0.9955
23.0	5.7342	1.0277	0.5443	1.0026	1.8136	5.1179	1.0029	0.9941
24.0	5.7525	1.0278	0.5524	1.0024	1.8183	4.9771	1.0036	0.9927

Table 3. Experimental Parameters with Temperatures in the Range of 293.15–423.15 K (20.2 MPa)

T (K)	C_s (10^4 mol/mL)	ρ (g/L)	Z	V_f/V_s	D_a (10^{-7} m ² /s)	D_m (10^{-9} m ² /s)	Ra	t_c
293	7.2989	1.0354	0.3896	1.0053	1.3353	3.0884	1.8438	0.2941
303	6.8427	1.0330	0.3966	1.0048	1.4042	3.3059	1.6434	0.3702
313	6.4892	1.0314	0.4066	1.0043	1.4741	3.5587	1.4844	0.4538
323	6.2497	1.0303	0.4213	1.0039	1.5454	3.8654	1.3637	0.5376
333	6.0216	1.0292	0.4426	1.0036	1.6172	4.2502	1.2549	0.6349
343	5.8391	1.0283	0.4717	1.0034	1.6915	4.7359	1.1639	0.7381
353	5.7251	1.0277	0.5089	1.0032	1.7653	5.3347	1.0932	0.8365
358	5.6840	1.0275	0.5308	1.00311	1.8037	5.6747	1.0624	0.8859
363	5.6886	1.0274	0.5523	1.00307	1.8413	6.0371	1.0412	0.9223
373	5.6909	1.0273	0.5971	1.00305	1.9172	6.7985	1.0000	1.0000
383	5.7023	1.0272	0.6419	1.00303	1.9957	7.6046	0.9629	1.0783
393	5.7137	1.0271	0.6867	1.00302	2.0744	8.4562	0.9281	1.1610

Effect of Temperature on Gravitational Convection.

Table 3 presents the CO₂ saturated solubility, density, compressibility factor, volumetric factor, average diffusion coefficient, molecular diffusion coefficient, normalized Rayleigh number, and normalized critical time with temperature varied in the range of 293.15–423.15 K.

Because of the reservoir pressure above the critical pressure of CO₂ (7.383 MPa), the CO₂ in liquid will be converted into the supercritical state when the temperature is beyond the critical point (304.21 K). For CO₂ in liquid, the saturated solubility in brine decreases with temperature. Because the Gibbs energy (G) increases with temperature (eq 18), dissolution reaches equilibrium earlier under higher temperature. For CO₂ in the supercritical state, the saturated solubility turns from decreasing to increasing with temperature, which is similar to the variation tendency of volumetric factor.

According to molecular dynamics, the molecular diffusion coefficient increases with temperature as $D_m \propto T^{3/2}$. The average diffusion coefficient also increases with temperature (Table 3) because all the diffusion coefficients of different ions increase with temperature.

The Rayleigh number depends on the excess density and diffusion coefficient, which are both affected by temperature. The temperature has a larger influence on diffusion coefficient than the density difference between CO₂ solution and brine at the reservoir conditions. Thus, the diffusion coefficient

increases with temperature to enhance the proneness to form gravitational convection.

Further Discussion in Numerical Simulation. This study has been applied to evaluate and predict the productivity of CO₂ flooding and the carbon storage in a Chinese oilfield. After long-term water flooding in this oilfield, the residual oil saturation was 30–35%, the water cut had already reached 98%, and the total recovery percentage had reached 51.52%, which was 99.46% of water flooding recoverable reserves in 2009. The CO₂ flooding has come into the phase of industrialized application since 2010 after its field experiment for 2 years. The CO₂ flooding was mainly conducted by crestal injection.

A precise reservoir geological modeling⁶⁰ was set up and applied (see Figure 6a,b). During the reservoir numerical simulation, a convective diffusion model was built based on our result and used to simulate the CO₂ diffusion in brine. The CO₂ diffusion in oil was simulated with a multicomponent diffusion model. Compared with traditional diffusion model, this model can result in dissolved CO₂ that tends to diffuse toward the bottom caused by gravitational convection, which has been proved by CO₂ production data (see Figure 6c,d).

CONCLUSIONS

Visualized experiments with a Hele-Shaw cell were performed to study the gravitational instabilities and their effect on

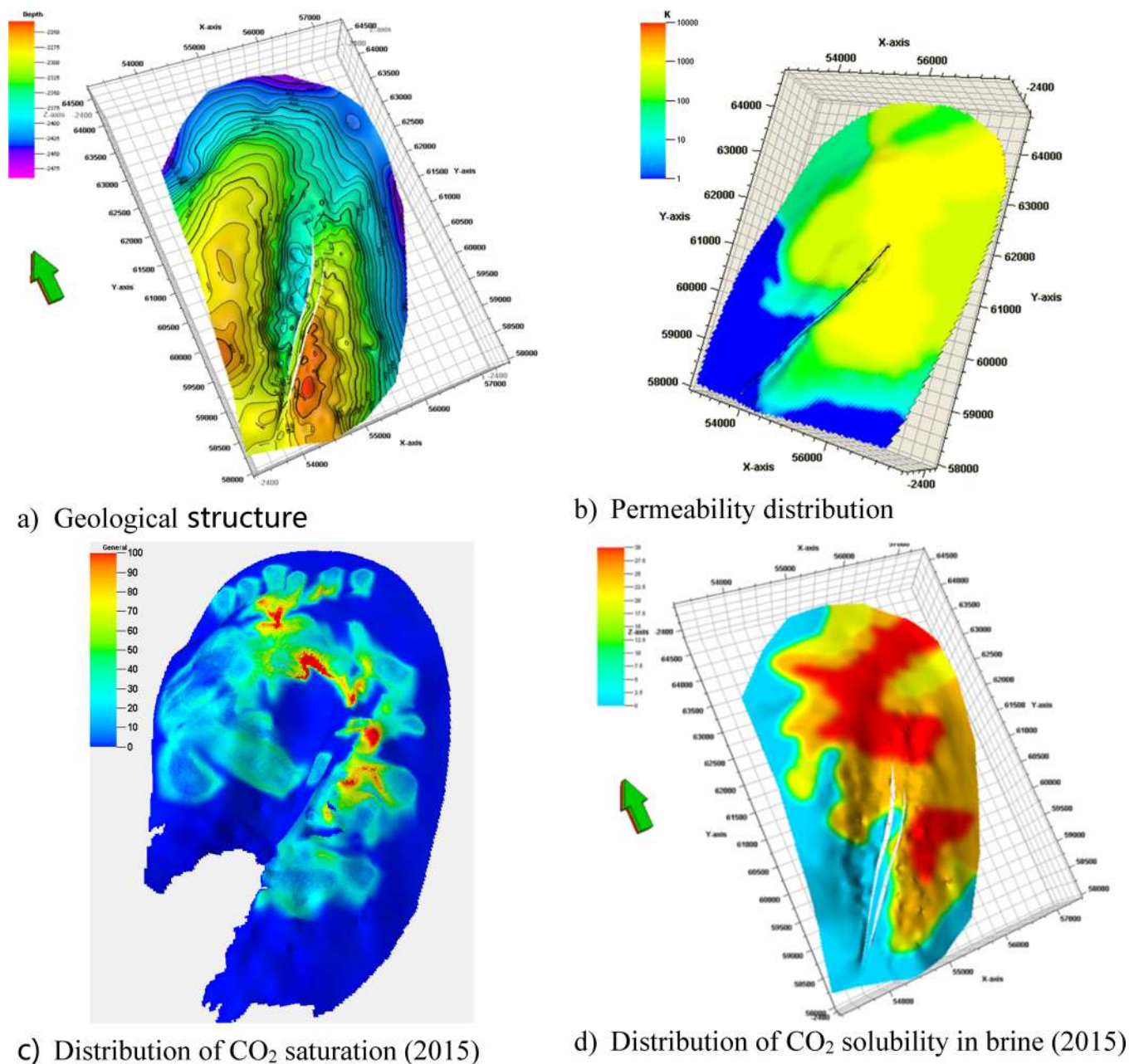


Figure 6. (a–d) Precise 3D reservoir model of Pucheng Oilfield built by Petrel with a grid step size of 50 m.

diffusion rate. The disturbances in the diffusive layer gradually boosted and expanded into convection under the gravitational instabilities. The convective currents triggered by density gradient remarkably enhanced the CO₂ dissolution rate. The density-driven convection further enhances the geological trapping potential. The quantitative experiments in a PVT cell were conducted to investigate the effect of density-driven convection on CO₂ diffusion coefficient by the constant-pressure method. The results demonstrate that the CO₂ diffusion coefficient peaks at early times via the natural convection and higher than the molecular diffusion coefficient. The CO₂ diffusion coefficient was then reduced to approach the average diffusion coefficient with time, which means that the natural convection decreases with time, similar to the density gradient. The PVT experiments were carried out at the temperatures of 293.15–423.15 K and pressures of 14–24 MPa to quantitatively test the influence of temperature or

pressure. The results imply that the Rayleigh number increases with pressure and the onset time decreases with pressure. The pressure has a larger influence on CO₂ solubility and density than diffusion coefficient at the reservoir conditions. Thus, the excess density increases with pressure to enhance the proneness to form gravitational convection. The temperature has a larger influence on the diffusion coefficient than the density difference between CO₂ solution and brine at the reservoir conditions. Thus, the diffusion coefficient increases with temperature to enhance the proneness to form gravitational convection. Therefore, the gravitational convection is more likely to occur under greater pressure or higher temperature.

■ EXPERIMENTAL SECTION

Materials and Conditions. The PVT testing was carried out under the formation conditions, with an average formation temperature of 355.65 K and formation pressures of 15–24 MPa (average, 20.2 MPa).² The scCO₂ used in this work is included in Table 4. Resident brine provided by the oilfield has

Table 4. CAS Registry Number and Mass Fraction Purity of Gas

component	CAS reg. no.	supplier	mass fraction
CO ₂	124-38-9	Beijing Huayuan Gas Chemical Industry Co., Ltd.	>0.990

a salinity of above 240 g/L. The ionic composition is listed in Table 5.² The viscosity tested with a VISCO 3-1000 LT viscometer (Core Laboratories S.T., USA) is 1.0903 mPa·s at standard conditions ($T = 293.15$ K, $P = 0.1$ MPa) and 0.5092 mPa·s at reservoir conditions (355.65 K, 20.2 MPa). The densities tested with density meters (Anton Paar, DMA HP) are 1.1989 g/mL at standard conditions and 1.0036 g/mL at reservoir conditions.

Visualization Experiments. To better understand the gravitational instabilities and convective instabilities, visualization experiments were conducted in a Hele-Shaw cell at reservoir conditions.³² The convective behavior in the Hele-Shaw cell is governed by the same law as in porous media.

Experimental Apparatus. A vertically oriented Hele-Shaw cell apparatus, rated to 70 MPa and 473.15 K, was designed independently to study the diffusion and convection characteristics of CO₂ qualitatively (in Figure 7). Similar to the microvisualization experiment apparatus,⁶¹ the Hele-Shaw cell apparatus consists of flat quartz models, a high-pressure holder, flow system, and image acquisition and analysis system. The models with a size of 8 cm × 8 cm × 4 mm have interior rectangular chambers with a size of 4 cm × 4 cm and cell aperture thickness (b) of 0.2 mm. For the Hele-Shaw model with uniform aperture thickness, the Rayleigh number (Ra) is 173.23, and the corresponding permeability (K) is 3333 μm^2 under the reservoir conditions (355.65 K, 20.2 MPa). The model remains vertical in the gravity field and is fitted rigidly in the pressure holder under surrounding pressure created by injecting deionized water. The model has a top outlet and bottom outlet to connect with the pressure holder. The injecting pressure, surrounding pressure, and back pressure were generated and controlled with Quizix pumps within ± 0.01 kPa. The temperature of the cell was measured with a calibrated thermocouple and controlled by an electric heating system within ± 0.01 K. The pressure holder has sapphire windows for visualization. The images are taken with a transmitted light image acquisition system composed of a Phantom Miro-M320S camera, microscope, LED light tablet, relative analysis software, etc. The image acquisition and analysis system is capable of recording 1320 frames per second (fps) at its resolution of 1920 × 1200 pixels.⁶¹

Experimental Procedure. After vacuuming the whole system, the pressure holder was filled with deionized water,

and the Hele-Shaw cell was filled with formation water from the bottom outlet. Before each measurement, the entire system had been heated to formation temperature (355.65 K). We injected CO₂ into the Hele-Shaw cell from the top outlet to form a CO₂–water interface at the upper of the model and discharged formation water from the bottom outlet back into the brine container. The camera was adjusted to keep the upper boundary of the visual area to coincide with the gas–water interface. The surrounding pressure and model pressure were pressurized to formation pressure (20.2 MPa) and remained constant with the Quizix pumps. Based on the advanced refraction imaging technique,³⁹ the CO₂ convection images were taken with the transmitted light imaging system. The CO₂ concentration images of high accuracy and resolution were inferred from transmitted light intensity according to the micro-schlieren technique.

Quantitative PVT Experiments. Experimental Apparatus. We used a PVT apparatus (Core Laboratories S.T., USA) to study the characteristics of CO₂ dissolution and diffusion in formation water at temperatures of 293.15–423.15 K and pressures of 14–24 MPa. The apparatus is illustrated in Figure 8. The PVT cell has a total sample volume of 240 mL and is rated to 150 MPa and 473.15 K.⁶² A visible sapphire window was attached to the front of the cell to obtain full visibility of all the contents, and a magnetic stirrer was equipped on the other side of the cell. The pressure generated with an automatic pump was tested with pressure sensors and controlled with a pressure regulator (CPS) within ± 10 kPa. The temperature of the PVT cell was measured by using a calibrated thermocouple and controlled with an electric heating system within ± 0.01 K. The volume of the gaseous phase in the PVT cell was measured with a camera-based measurement system (CCD) with the accuracy of 0.0001 mL. We used a GAS 4000 gasometer (Core Laboratories S.T., USA) with 0.001 mL resolution to accurately measure the gas volume at atmospheric pressure.

Experimental Procedure. For quantitative analysis of the CO₂ diffusion, the diffusion of CO₂ in resident brines is tested with the constant-pressure method to provide more accurate (within 0.01%⁶²) results by taking into account the liquid phase swelling⁴ and unaffected by CO₂ compression.⁴⁷ For the constant-pressure method, the diffusion coefficient is calculated by the changes in volume recorded during CO₂ dissolution and diffusion at constant temperature and pressure.^{63–66}

Before starting, a leakage test with nitrogen gas was done to ensure that there is no leakage in the system. The formation water and CO₂ were heated to experimental temperature and pressurized to experimental pressure. After vacuuming the system's inner space, a given volume of formation water sample was pressurized into the vertical PVT cell under experimental pressure. Meanwhile, the cell was loaded with the same pumping speed. A sufficient amount of CO₂ was then injected into the PVT cell under experimental conditions. After stopping CO₂ from drawing in, the carried pressure remained constant via the precision pressure regulator. The volume (V) of the cell was measured with CCD system and continuously

Table 5. Ionic Composition of Formation Water (mg/L)

Na ⁺ , K ⁺	Ca ²⁺	Mg ²⁺	Cl ⁻	SO ₄ ²⁻	HCO ₃ ⁻	CO ₃ ²⁻	total
90,452	32,989	4325	92,440	6985	8985	967	243,143

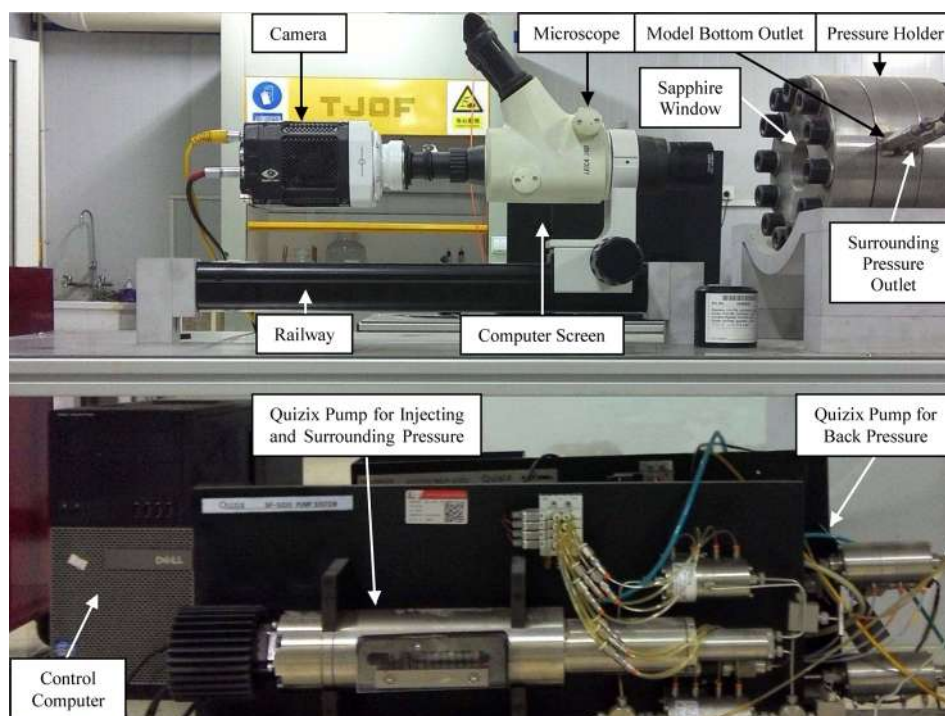


Figure 7. Photograph of the Hele-Shaw cell apparatus.

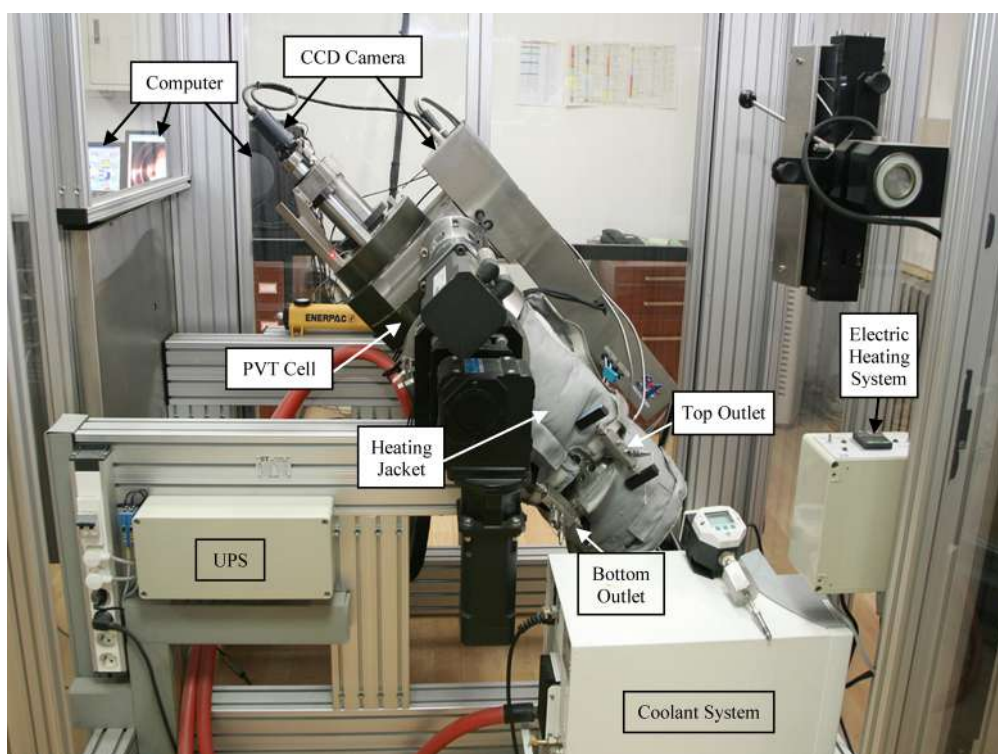


Figure 8. Photograph of the PVT apparatus.

recorded.⁶² Some gas phase samples were taken from a top valve with a vacuumed 1 mL flash separator tank (FST). After the tank with the sample was cooled in the water bath, the gas volume at atmospheric pressure was measured with the gasometer for calculating the compressibility factor (Z_t). The gasometer was connected to a gas chromatography spectrometer (Waters, USA) for measuring CO_2 volume concentration in gas (c_t). The diffusion experiment was maintained until the

system had reached a thermodynamic equilibrium, as indicated by the volume. Some liquid phase samples were taken from a bottom valve and slowly charged into a vacuumed FST. During the charging process, a needle backpressure valve (with a dead volume of 0.178 mL) was used to avoid pressure decrease. The charged liquid sample (M) was weighted using a precision balance (Mettler Toledo, USA) with an accuracy of 0.001 g for calculating the density (ρ). After cooling in the water bath, the

gas volume (V_{s0}) was measured with the gasometer at atmospheric pressure. The CO_2 concentration in evolved gases (c_i') was measured with the gas chromatography spectrometer (Waters, USA).

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Notes

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